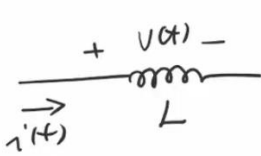
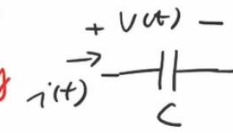


L. C.



passive components
 Cannot generate energy
 Store energy



Store/release energy in
 the form of "i", Mag. field.

energy in
 the form of "v", elet. field.

i cannot jump

v cannot jump.

Time domain:

$$v(t) = L \cdot \frac{di(t)}{dt}$$

$$i(t) = C \frac{dv(t)}{dt}$$

$$i(t) = \frac{1}{L} \int_0^t v(x) dx + i(0)$$

$$v(t) = \frac{1}{C} \int_0^t i(x) dx + v(0)$$

freq. domain:

$$\checkmark Z_L = j\omega L$$

\downarrow
 $2\pi f$

$$\checkmark Z_C = \frac{1}{j\omega C} = -\frac{j}{\omega C}$$

\uparrow
 $2\pi f$

DC: $f=0$, short

$f \geq 0$, open.

AC: $f \rightarrow \infty$, open

$f \rightarrow \infty$, short

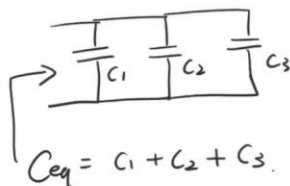
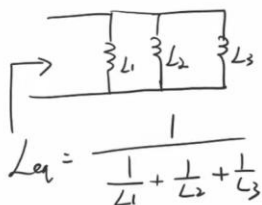
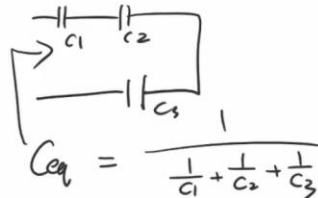
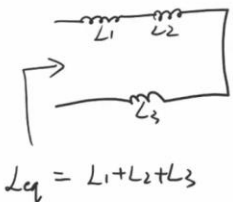
→ RL, RC, RLC step response with DC source.

→ AC analysis, "w", "f"

AC analysis:

$i(t)$ lags $v(t)$ by $90^\circ/\frac{\omega}{2}$.

$i(t)$ leads $v(t)$ by $90^\circ/\frac{\omega}{2}$.





$$X(t) = X_F + (X_0 - X_F) \cdot e^{-\frac{t}{\tau}}$$

Sep/Natural Response.

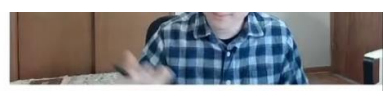
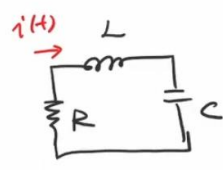
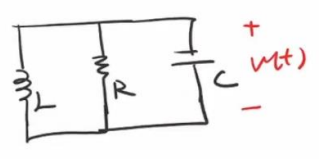
DC steady-state



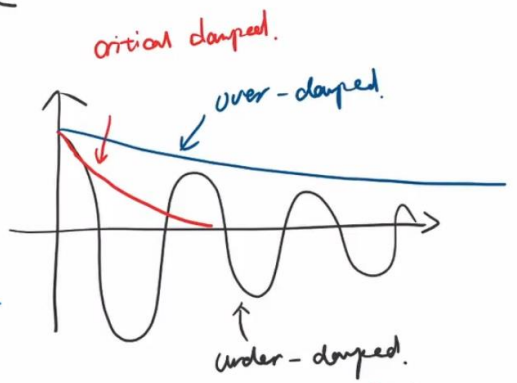
$$\tau = \frac{L}{R}$$

$$\tau = RC$$

RLC



Natural: $\alpha^2 > \omega_0^2$, over damped condition
 $\alpha^2 = \omega_0^2$, critical damped
 $\alpha^2 < \omega_0^2$, under damped



$$\alpha = \frac{1}{2RC}$$

$$\omega_0 = \frac{1}{\sqrt{LC}}$$

$$\alpha = \frac{R}{2L}$$

$$\omega_0 = \frac{1}{\sqrt{LC}}$$

$$\rightarrow X(t) = A_1 e^{s_1 t} + A_2 e^{s_2 t}, t \geq 0. s_1 = -\alpha + \sqrt{\alpha^2 - \omega_0^2}, s_2 = -\alpha - \sqrt{\alpha^2 - \omega_0^2}, X(0) = A_1 + A_2, \frac{dX(0)}{dt} = A_1 s_1 + A_2 s_2$$

$$\rightarrow X(t) = D_1 t e^{-\alpha t} + D_2 e^{-\alpha t}, t \geq 0. X(0) = D_2, \frac{dX(0)}{dt} = D_1 - \alpha D_2$$

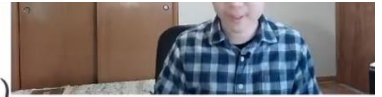
$$\rightarrow X(t) = e^{-\alpha t} (B_1 \cos \omega_d t + B_2 \sin \omega_d t), \omega_d = \sqrt{\omega_0^2 - \alpha^2}$$

$$X(0) = B_1, \frac{dX(0)}{dt} = -\alpha B_1 + \omega_d B_2$$

Sep:

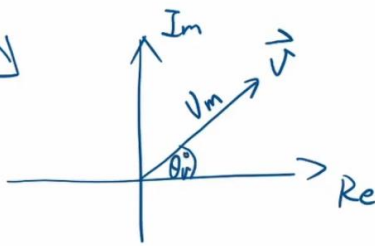
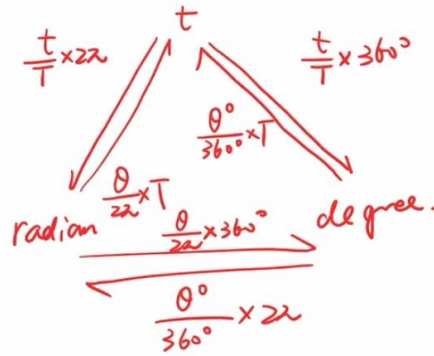
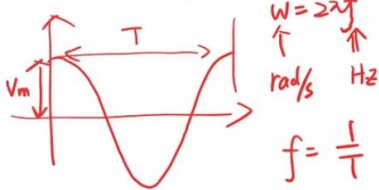
$$X(t) = X_F + \{ \text{Natural Response} \}$$

Sinusoidal Response.



$$v(t) = V_m \cos(\omega t + \theta_v), \quad i(t) = I_m \cos(\omega t + \theta_i)$$

Amplitude \uparrow \uparrow freq. \uparrow initial phase \uparrow



$$\mathcal{P}\{v(t)\} = V_m \angle \theta_v = V_m \angle \theta_v = V_m e^{j\theta_v} = \vec{V}$$

$$V_{rms} = \frac{V_m}{\sqrt{2}}, \quad I_{rms} = \frac{I_m}{\sqrt{2}}, \quad (\text{for sinusoidal signals})$$

$$V_{rms} = \sqrt{\frac{1}{nT} \int_0^{nT} v^2(t) dt}$$

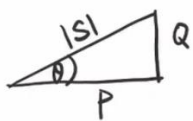
$$Z_L = j\omega L, \quad Z_C = \frac{1}{j\omega C} = -\frac{j}{\omega C}$$

$$Z = R + jX$$

do AC Analysis with what we learned in DC Analysis:
 KCL, KVL, Node-voltage, Mesh-current, Source-transformation
 Thevenin/Norton eqn.

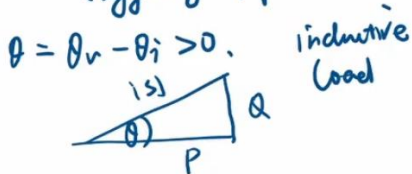
$$\underline{S} = P + jQ$$

App. Real Reant

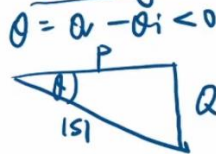


$\theta = \theta_v - \theta_i$: PF Angle, $\cos(\theta_v - \theta_i) = PF$. PF \rightarrow 1, better

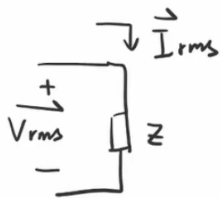
(lagging PF)



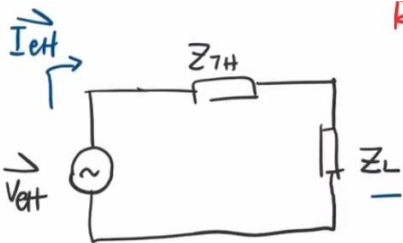
(leading PF)



$$\vec{S} \neq \vec{V} \times \vec{I}, \quad \vec{S} = \frac{\vec{V} \times \vec{I}^*}{2}, \quad \vec{S} = \vec{V}_{rms} \cdot \vec{I}_{rms}^* = \vec{V}_{eff} \cdot \vec{I}_{eff}^*$$



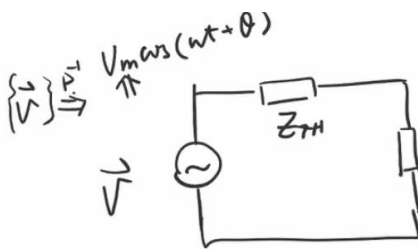
$$S_Z = \vec{V}_{rms} \cdot \vec{I}_{rms}^* = |\vec{I}_{rms}|^2 \cdot Z = \frac{|\vec{V}_{rms}|^2}{Z}$$



$R_{TH} = R_L$

$$Z_L = Z_{TH}^*, \quad Z_L = R_{TH} - jX_{TH}$$

$$P_{max-L} = |\vec{I}_{eff}|^2 \cdot R_L = \left(\frac{|\vec{V}_{eff}|}{2R_{TH}} \right)^2 \cdot R_L = \frac{|\vec{V}_{eff}|^2}{4R_{TH}} = \frac{|\vec{V}_{eff}|^2}{4R_L}$$



$$|\vec{V}_{eff}| = \frac{V_m}{\sqrt{2}}$$

$$P_{max-L} = \frac{V_m^2}{8R_L} = \frac{V_m^2}{8R_{TH}}$$